

## Structural Changes in the Carbon Black Network in Carbon-Black-Filled Styrene-Butadiene Rubber Samples Cured with a Two-Step Process

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**ABSTRACT:** The volume resistivity of carbon black (CB)-filled crosslinked styrene-butadiene rubber (SBR) samples cured in two steps and having a fixed elongation condition declined slightly when the elongation ratio ( $\alpha$ ) was 3 or smaller, whereas the value increased markedly at  $\alpha = 4$ . Three-dimensional transmission electron microscopy observations revealed that the closest interparticle distance between the carbon black aggregates ( $CB_{ag}$ 's) and the  $CB_{ag}$  number density decreased at  $\alpha = 1-2$  but increased at  $\alpha = 4$  and that the distance between the centers of gravity of the closest  $CB_{ag}$  and the volume of  $CB_{ag}$  increased at  $\alpha = 1-3$  but decreased at  $\alpha = 4$ . Also, the fraction of crosslinked chains of the carbon black network ( $CB_{net}$ ) was decreased with elongation, and the fraction of branched chains increased. The fraction of isolated chains in particular showed a more pronounced increase at  $\alpha > 3$  compared with  $\alpha < 3$ . These results presumably imply that for the sample with  $\alpha > 3$ , the coarsened  $CB_{ag}$ 's were finely divided and also that the  $CB_{net}$  was broken by elongation. © 2012 Wiley Periodicals, Inc. *J. Appl. Polym. Sci.* 000: 000–000, 2012

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### INTRODUCTION

Polymer nanocomposites are unique materials in that their material properties change substantially with the addition of a small volume fraction of nanometer-sized filler particles.<sup>1–6</sup> The changes are observed when the filler size is comparable to that of the polymer chains and to the average wall-to-wall distance between fillers. Under such conditions and with good filler dispersion in the matrix, it is believed that a secondary network of polymer chains connecting the filler particles forms.<sup>2–5</sup> This transient network is assumed to be the cause of the large enhancement observed in the viscoelastic properties. The transient network also produces rubberlike behavior in a certain range of frequencies.<sup>3</sup> The appearance and range of this regime depend on the polymer–filler affinity and, hence, on the lifetime of attachments between the fillers and bridging chains.

It has been reported in recent years that an electrical network forms among carbon black aggregates ( $CB_{ag}$ 's) in sulfur-cured natural rubber (NR) vulcanizates when the carbon black (CB) filler content is 30 phr (grams of additive per 100 g of rubber) or higher.<sup>7–12</sup> This finding is based on the measurement of the closest interparticle distance ( $d_p$ ) of the  $CB_{ag}$ 's with three-dimensional (3D) transmission electron microscopy (TEM)

observations, image analysis, and volume resistivity ( $\rho_v$ ) measurements. These techniques have revealed many new insights, including that the structures of the carbon black network ( $CB_{net}$ ) consist mainly of crosslinked chains and branched chains and that a certain relationship exists between the fractions of these chains and the CB filler content. Furthermore, two dielectric relaxation components (a circular arc shaped pattern and the remaining relaxation) were isolated from Cole–Cole plots of dielectric relaxation, and a good linear relationship was found to exist between the chain fractions and the fractions of the intensities of these relaxation components.<sup>9</sup> Omnès et al.<sup>13</sup> also suggested that the elastic modulus of CB-filled sulfur-cured NR vulcanizates can be predicted with a morphological model that takes into account bound rubber, occluded rubber, and also the structures of the filler network.

Meanwhile, on the basis of  $q_v$  measurements and 3D TEM observations, Kato et al.<sup>14</sup> reported that the  $CB_{net}$  in CB-filled crosslinked NR was destroyed when the heat treatment conditions were set to minimize the occurrence of thermal oxidative degradation. It was found that the crosslinked chains of the  $CB_{net}$  were broken by the heat treatment process and that the number of branched chains increased. These findings showed

**Table I.** Recipes for the Preparation of the CB-Filled Cured SBR Reference Samples and the Sample Cured in Two Steps

Sample	Ingredients					
	CB10/SBR <sup>a</sup>	CB20/SBR <sup>a</sup>	CB40/SBR <sup>a</sup>	CB60/SBR <sup>a</sup>	CB80/SBR <sup>a</sup>	CB40/SBR ( $\alpha$ ) <sup>b</sup>
SBR1502	100	100	100	100	100	100
DCP (phr) <sup>c</sup>	3	3	3	3	3	3
CB (phr) <sup>d</sup>	10	20	40	60	80	40
$\Phi_{CB}$ <sup>e</sup>	0.050	0.095	0.17	0.24	0.30	0.17

<sup>a</sup>Curing conditions: 30 min at 170°C under pressure of 2 MPa.

<sup>b</sup>Two-step curing conditions: (1) precuring for 8.5 min at 130°C under a pressure of 2 MPa before elongation and (2) postcuring for 15 min at 170°C after elongation.

<sup>c</sup>Grams per 100 g of rubber.

<sup>d</sup>High abrasion furnace (N330).

<sup>e</sup>Calculated with densities of CB and SBR of 1.8 and 0.94.

that 3D TEM observations and image analysis are effective techniques for examining the structural changes that occur in the  $CB_{net}$ . Satoh et al.<sup>15</sup> measured the differential dynamic modulus (DDM) and  $\rho_v$  values of CB-filled uncured SBRs (i.e., CB-filled SBR compounds) in a wide range of shear strains from 0.001 to 0.5. They found that there was a one-to-one correspondence between the changes in DDM and  $\rho_v$  above the percolation threshold; that is, there was no  $\rho_v$  change in the linear viscoelasticity, but there was a  $\rho_v$  enhancement in the nonlinear viscoelasticity. These results mean that the contact CB filler network exists and the nonlinear viscoelasticity of high-CB-filled rubber is caused by a rupture in the CB filler network. In addition, on the basis of the measurements of DDM in large compression and recovery, they found that the filler network ruptured because of large compression and recovery in shape was attained at a timescale that was closely related to the particle size.<sup>16</sup>

Many of the experimental findings mentioned previously suggested change and recovery in the CB–filler network in large deformation. Now, we have very powerful tools in 3D TEM and the image analysis technique, which give us direct observation of the CB–filler network structure. Therefore, in this study, the change in  $\rho_v$  and the structural change in the stretched  $CB_{net}$  in CB-filled cured styrene-butadiene rubber (SBR) specimens prepared by a two-step curing method were investigated on the basis of  $\rho_v$  measurements, 3D TEM observations, and image analysis.

## EXPERIMENTAL

### Materials: CB-Filled SBR Cured in Two Steps

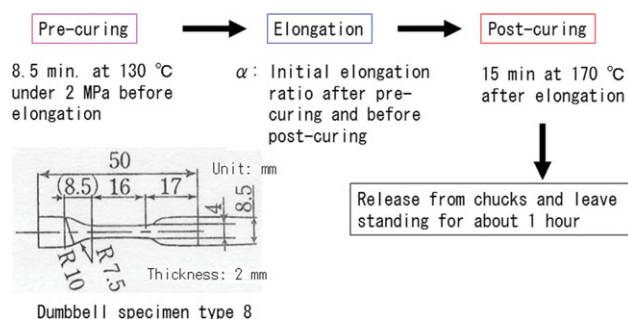
Two types of CB-filled cured SBR 1502 were prepared: reference samples and samples cured in two steps. The compounding recipes of the reference samples investigated in this study are given in Table I. The only ingredient that changed in the series of cured SBR samples was the CB loading, which was varied in the range 10–80 phr. The carbon black volume fraction ( $\Phi_{CB}$ ) was calculated with densities of CB<sup>17</sup> and SBR<sup>18</sup> of 1.8 and 0.94 g/cm<sup>3</sup>, respectively. The quantity of the compounding agent was the same in all of the cured samples: 3 phr of dicumyl peroxide (DCP). Curing was performed under a pressure of 2 MPa at 170°C for 30 min in a mold.

Table I shows the recipes of the CB-filled SBR 1502 samples cured in two steps, and Figure 1 shows the curing process. The DCP and CB loadings were 3 and 40 phr, respectively. Precuring was per-

formed under a pressure of 2 MPa at 130°C for 8.5 min in a mold. Rectangular specimens (50 mm wide, 70 mm long, and 2 mm thick) were cut from precured SBR sheets. After stretching, the specimens between two marker lines at an arbitrary elongation ratio ( $\alpha$ ), and the stretched specimens were postcured at 170°C for 15 min. After postcuring, the specimens were released from the chucks and held at room temperature for about 1 h before we measured the distance between the two marker lines.  $\alpha$  is defined here as the ratio of the length of the specimen before extension to the length of the specimen after extension. Table II shows the residual elongation ratios ( $\alpha_{res}$ ) of the CB-filled CB40/SBR samples after two steps of curing (where  $\alpha$  is the initial elongation ratio from 1 to 4 after precuring and before postcuring). The  $\alpha_{res}$  values of the specimens were 90% or more of the initial  $\alpha$  values. Taking into consideration the findings of Kohjiya et al.,<sup>7,8,11,12</sup> Kato et al.,<sup>9,14</sup> Ikeda et al.,<sup>10</sup> and Satoh et al.,<sup>15</sup> we believe that a  $CB_{net}$  also formed in the CB40/SBR samples in this study, despite the different kinds of CB and rubber used and the differences in the vulcanizing or curing systems.

### Apparatus and Procedure

**Measurement of  $\rho_v$ .** The  $\rho_v$  values of the samples were measured with the three-electrode method with an R8340A ultra-high-resistance meter (Advantest Corp., Tokyo, Japan). The three electrodes were made of stainless steel and consisted of a main electrode 50 mm in diameter, a guard electrode with internal/external diameters of 70/80 mm and a counter electrode 103 mm in diameter (TR-43C, Advantest Corp.) An SBR sample cured in two steps was tightly sandwiched between the main



**Figure 1.** Two-step curing process of the CB-filled cured SBR samples. [Color figure can be viewed in the online issue, which is available at [wileyonlinelibrary.com](http://www.wileyonlinelibrary.com).]

**Table II.**  $\alpha_{res}$  Values of the CB-Filled Cured SBR Samples ( $\alpha = 1-4$ ) after Two Steps of Curing

Sample	CB40/SBR ( $\alpha = 1$ )	CB40/SBR ( $\alpha = 2$ )	CB40/SBR ( $\alpha = 3$ )	CB40/SBR ( $\alpha = 4$ )
$\alpha$	1	2	3	4
$\alpha_{res}$	1	1.82	2.82	3.77

and guard electrodes and the counter electrode. The guard electrode was grounded to prevent current from flowing along the sample surface.  $\rho_v$  was calculated from the current that flowed through the sample when a certain specified voltage was applied. This measurement method conformed to the procedure specified in the relevant Japanese Industrial Standard (JIS K 6911), which is equivalent to ASTM D 257-90. The sample cells were also loaded in a constant-temperature bath, which was used to keep the temperature at a specified level for approximately 20 min. The range of temperature measurement was from 296 to 363 K (23–90°C), and the applied voltage was 100 or 1 V/min. Subsequently, the current that flowed through the sample upon the application of voltage was measured to determine the temperature dependence of  $\rho_v$ .

**3D TEM Observations.** The instrument used in the 3D TEM observations was a Tecnai G2 F20 TEM (FEI Co., Hillsboro, Oregon, USA). The accelerating voltage of the electron beam was set at 200 kV. The samples were tilted over a range of angles from  $-70$  to  $+70^\circ$ , and image data (tilted images) were continuously obtained in  $2^\circ$  increments. In total, 71 consecutive tilted images were automatically loaded into the computer. The positions of the tilted images were aligned at that time, and a search was made for their axis of rotation. These tilted images were not simply two-dimensional image slices but rather two-dimensional projected images of the mass–density distribution of the samples. Using IMOD software (a program created at Colorado University)<sup>19</sup> installed on the TEM, we converted the

consecutive tilted images thus obtained into image slices showing the mass–density distribution at each angle. Then, 3D images were reconstructed from the image slices by application of a radon transform with the Amira software developed by TGS, Inc, Irvine, California, USA.<sup>20</sup>

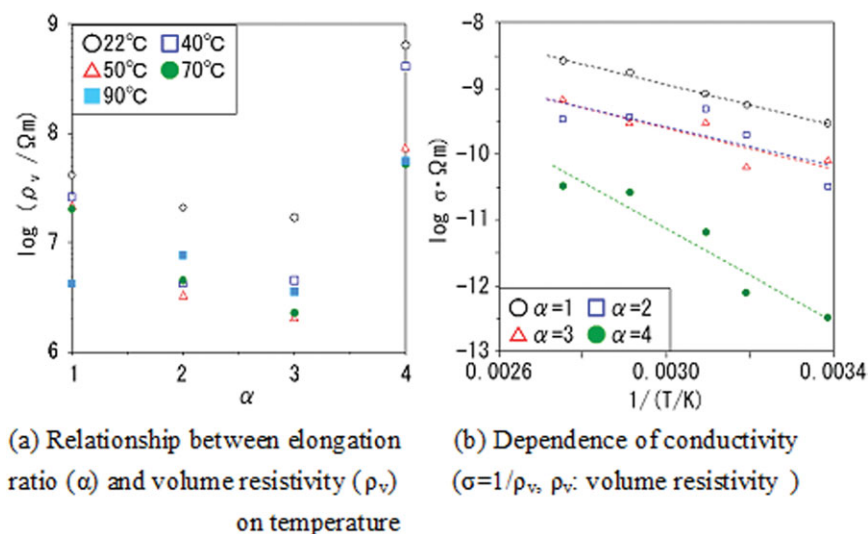
Simultaneously, volume rendering or surface rendering was performed to construct the 3D images on a nanometer scale.<sup>21</sup> The former method reconstructs a 3D object by stacking cross-sectional images vertically and displaying the data semitransparently. The latter method reconstructs a 3D object by extracting the contours of the object depicted in a cross-sectional image in terms of curves and inserting surfaces between many of the curves thus obtained.

The principle of 3D TEM is virtually the same as that of X-ray computed tomography. Because an electron beam is used, this technique is also called *electron beam tomography*. The use of 3D TEM not only facilitates the 3D visualization of nanoparticles, it also makes it possible to calculate their number, density, 3D shape, volume, and other details.<sup>7–12,22–28</sup> Because it is well known that organic polymers are apt to be damaged by electron beams,<sup>29</sup> this is an issue that must always be kept in mind when one makes 3D TEM measurements.

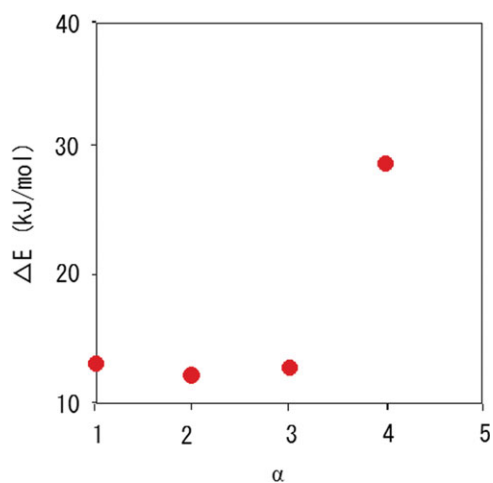
## RESULTS AND DISCUSSION

### Relationship between the $\rho_v$ and Temperature of the SBR Cured in Two Steps

Figure 2(a) shows the  $\rho_v$ 's measured in a temperature range of 22–90°C for the CB-filled crosslinked SBR samples having fixed  $\alpha$ s of 1–4, respectively. At 22°C, the samples with  $\alpha$ s of 1–3 showed a slight decline in  $\rho_v$  with increasing  $\alpha$ , whereas  $\rho_v$  increased markedly at  $\alpha = 4$ . This slight decline in  $\rho_v$  at  $\alpha = 1-3$  and the pronounced increase at  $\alpha = 4$  presumably occurred because of the changes in the distribution of the CB<sub>ag</sub>'s. These characteristics are described in more detail later, in the discussion of the 3D TEM observations. Moreover, all of the samples showed a decline in  $\rho_v$  with increasing temperature; this was



**Figure 2.**  $\sigma$  values of the CB-filled SBR samples cured in two steps. [Color figure can be viewed in the online issue, which is available at [www.interscience.wiley.com](http://www.interscience.wiley.com).]

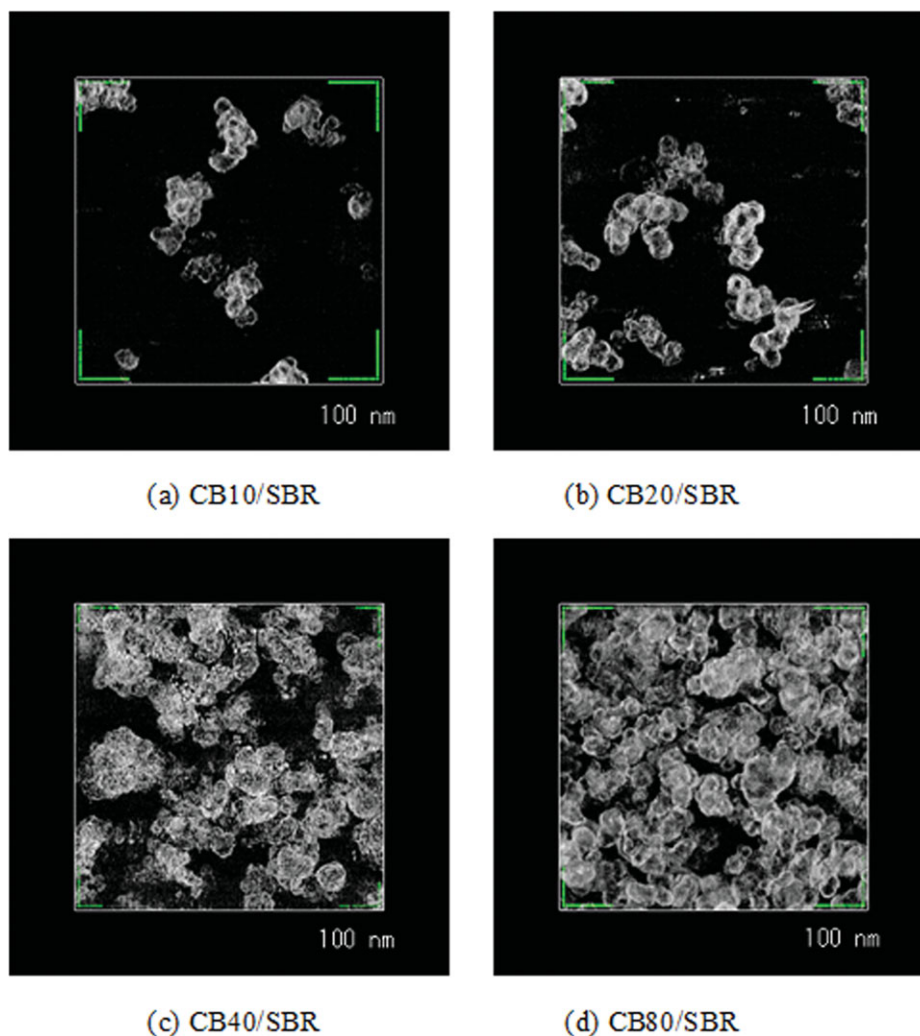


**Figure 3.** Relationship between  $\Delta E$  of  $\sigma$  and  $\alpha$ . [Color figure can be viewed in the online issue, which is available at [wileyonlinelibrary.com](http://wileyonlinelibrary.com).]

attributed to the process of thermal activation. Figure 2(b) presents Arrhenius plots, which show the logarithm of the electrical conductivity ( $\sigma = 1/\rho_v$ ) plotted against the inverse of the absolute temperature ( $T$ ). For all of the samples with  $\alpha$ s of 1–4, a nearly linear relationship was seen between  $\log \sigma$  and  $1/T$ . The activation energy ( $\Delta E$ ) of this conductivity could be found from the gradient of the straight-line approximations in the figure. Figure 3 shows  $\Delta E$  as a function of  $\alpha$ . For the samples with  $\alpha$ s of 1–3,  $\Delta E$  was low and was nearly the same in all three cases, but for the sample with an  $\alpha$  of 4,  $\Delta E$  was markedly higher. These results suggest that at  $\alpha = 4$ , that is, for an  $\alpha$  larger than 3, the electrical network of the  $CB_{ag}$ 's in the rubber was destroyed.

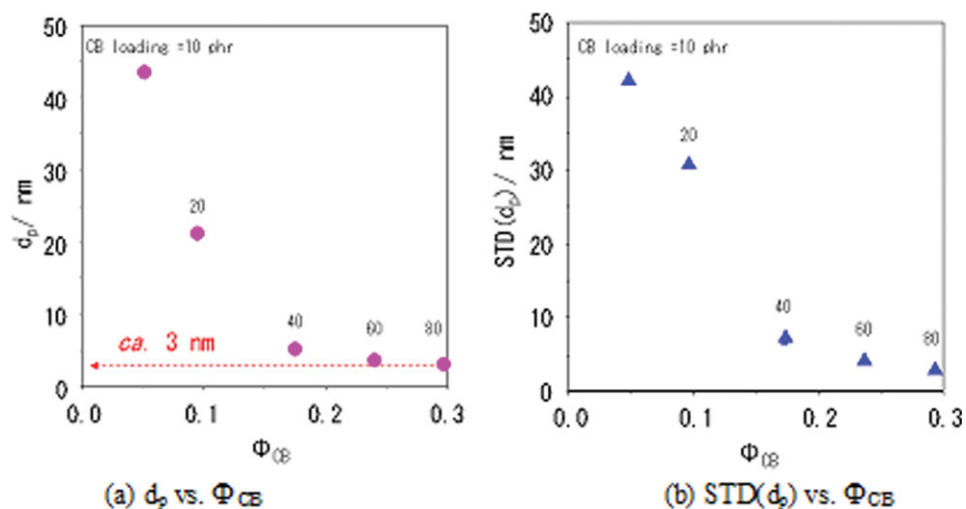
#### Distribution of the $CB_{ag}$ 's in the Reference Specimens and the Specimens Cured in Two Steps

Figure 4 shows 3D TEM images of the CB10, CB20, CB40, and 80/SBR reference samples. The white grains are  $CB_{ag}$ 's. In the CB10/SBR sample,  $CB_{ag}$ 's were observed here and there in the image. At CB loadings higher than 10 phr, the  $CB_{ag}$  structures continued to grow larger in size and tended to be nearly



**Figure 4.** 3D TEM images of the CB-filled cured SBR reference samples. [Color figure can be viewed in the online issue, which is available at [wileyonlinelibrary.com](http://wileyonlinelibrary.com).]





**Figure 5.** Dependence of the average closest  $d_p$  between the  $CB_{ag}$ 's and  $STD(d_p)$  on  $\Phi_{CB}$ . [Color figure can be viewed in the online issue, which is available at [wileyonlinelibrary.com](http://wileyonlinelibrary.com).]

uniformly distributed in the CB80/SBR samples. By applying a 3D image analysis technique to the images in Figure 4, we determined the closest  $d_p$  between  $CB_{ag}$ 's and its standard deviation [ $STD(d_p)$ ], as proposed by Kato and coworkers.<sup>7–12,14,24,26,27</sup>

Figure 5(a, b) shows the dependence of  $d_p$  and  $STD(d_p)$  on  $\Phi_{CB}$ , respectively. It is seen in Figure 5(a, b) that  $d_p$  and  $STD(d_p)$  decreased as  $\Phi_{CB}$  increased above 0.050 (10 phr) and that both values stabilized at  $\Phi_{CB}$ 's of 0.17 (40 phr) or higher. The stable value of  $d_p$  was approximately 3 nm, which was identical to the value reported for high abrasion furnace-filled sulfur-cured NR vulcanizates.<sup>7–12,14,24,26,27</sup> These results imply the presence of a CB/SBR interaction layer that prevented direct contact between the  $CB_{ag}$ 's even when  $\Phi_{CB}$  was increased. We assumed that this interaction layer was closely related to the bound rubber phase. As described later, the linking of the  $CB_{ag}$ 's at a distance of 3 nm resulted in the formation of a  $CB_{net}$  consisting of crosslinked, branched, and isolated chains. In Figure 5(b), which shows the dependence of  $STD(d_p)$  on  $\Phi_{CB}$ , we observed that the  $CB_{ag}$ 's became more uniformly distributed at  $\Phi_{CB}$  values above 0.050 and that the samples were filled with CB at approximately the distance of the CB/SBR interaction layer at  $\Phi_{CB}$  of 0.17 or higher.

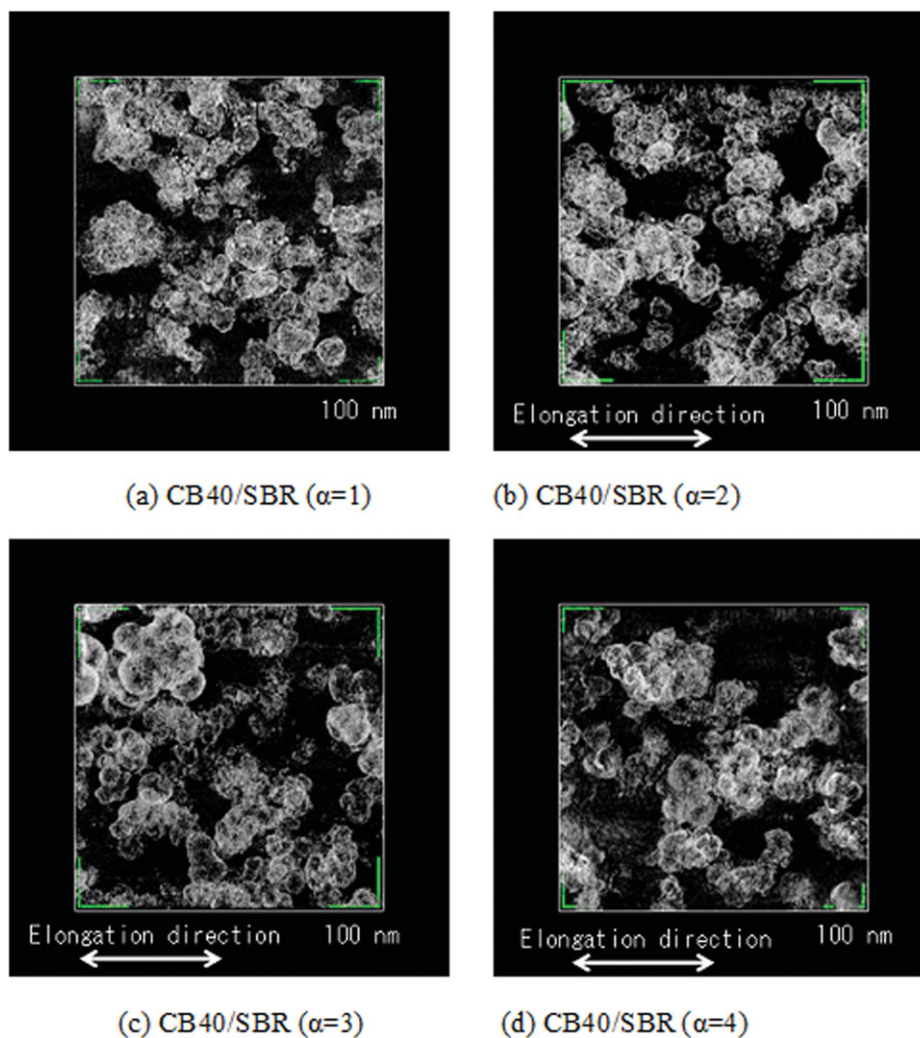
Figure 6 shows the 3D TEM images of the CB40/SBR samples cured in two steps and having  $\alpha$  values in the range 1–4. The elongation direction is along the horizontal axis, and the white grains are  $CB_{ag}$ 's. We observed that the gaps between the  $CB_{ag}$ 's tended to increase with increasing  $\alpha$ . In particular, at  $\alpha = 4$ , the  $CB_{ag}$ 's exhibited a segmented morphology. These results presumably support the pronounced increase seen in  $\rho_v$  for  $\alpha = 4$ . Figure 7 shows  $d_p$  and the distance between the centers of gravity of the closest carbon black aggregates ( $d_g$ 's) as a function of  $\alpha$ .<sup>7–12,14,24,26,27</sup> Surprisingly, the  $d_p$  values of the samples with  $\alpha$ s of 1–2 decreased slightly, whereas it increased for the samples with a larger  $\alpha$  value. These results imply that for the samples with  $\alpha$ s of 1–2, their cross-sectional area decreased with elongation and, thereby, pushed the  $CB_{ag}$ 's toward the interior of the sample. This resulted in a highly packed state that reduced  $d_p$

slightly;  $\rho_v$  also declined somewhat. At  $\alpha$  values greater than 2, the elongation probably pulled the  $CB_{ag}$ 's apart. This resulted in a pronounced increase in  $d_p$ ;  $\rho_v$  also increased markedly.

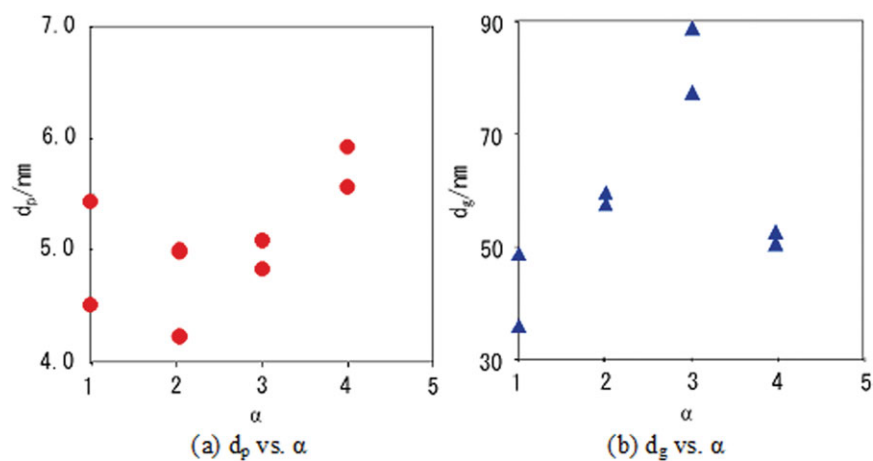
Furthermore, we observed that  $d_g$  increased at  $\alpha = 1–3$  and decreased at  $\alpha = 4$ . Here, we consider that  $d_g$  reflected  $d_p$  and the size of the two closest  $CB_{ag}$ 's. For the samples with  $\alpha = 1–3$ , the reduction of the sample cross-sectional area accompanying elongation promoted the coalescence of the  $CB_{ag}$ 's, whereas with an  $\alpha$  value greater than 3, the shear fields produced by the further reduction of the sample cross-sectional area presumably worked to finely divide the coarsened  $CB_{ag}$ 's. The dependence of the aggregate number density ( $D_{CB}$ ) and the average aggregate volume ( $V_{CB}$ ) on  $\alpha$  is shown in Figure 8. We observed that  $D_{CB}$  decreased with  $\alpha$  values of 1–3 and increased at  $\alpha = 4$ . The former result corresponded to the coalescence of the  $CB_{ag}$ 's, and the latter result corresponded to the division of the coarser  $CB_{ag}$ 's. In addition,  $V_{CB}$  increased at  $\alpha$  values of 1–3 and decreased at  $\alpha = 4$ . These results also corresponded well to the  $CB_{ag}$  coalescence and the division of coarser  $CB_{ag}$ 's.

#### **$CB_{net}$ in the Reference Specimens and the Specimens Cured in Two Steps**

The results in Figure 5 show that  $d_p$  displayed a constant value of approximately 3 nm when the CB loading was increased to 40 phr or higher. Because this value implied the thickness of the CB/SBR interaction layer, we assumed that the linking of the nearest neighbor  $CB_{ag}$ 's at a distance of approximately 3 nm formed the  $CB_{net}$ . Accordingly, the  $CB_{net}$  could be visualized by the drawing of lines connecting the centers of gravity of these nearest  $CB_{ag}$ 's.<sup>7–12,14,24,26,27</sup> Figure 9 presents images of the  $CB_{net}$  thus obtained for the CB40/SBR samples cured in two steps with  $\alpha$  values of 1–4, respectively. The elongation direction was along the horizontal axis, and bars representing 100 nm are shown in the four corners of each rectangular parallelepiped view.  $CB_{net}$ 's that are not connected are shown in different colors. The  $CB_{net}$  in the unelongated state ( $\alpha = 1$ ), shown in Figure 9(a), was almost entirely the same color; this indicated that nearly all of the  $CB_{ag}$ 's were linked at a distance of approximately 3 nm. In



**Figure 6.** 3D TEM images of the CB-filled SBR samples cured in two steps. [Color figure can be viewed in the online issue, which is available at [wileyonlinelibrary.com](http://wileyonlinelibrary.com).]



**Figure 7.** Average closest  $d_p$  between  $CB_{ag}$ 's and  $d_g$  as a function of  $\alpha$ . [Color figure can be viewed in the online issue, which is available at [wileyonlinelibrary.com](http://wileyonlinelibrary.com).]

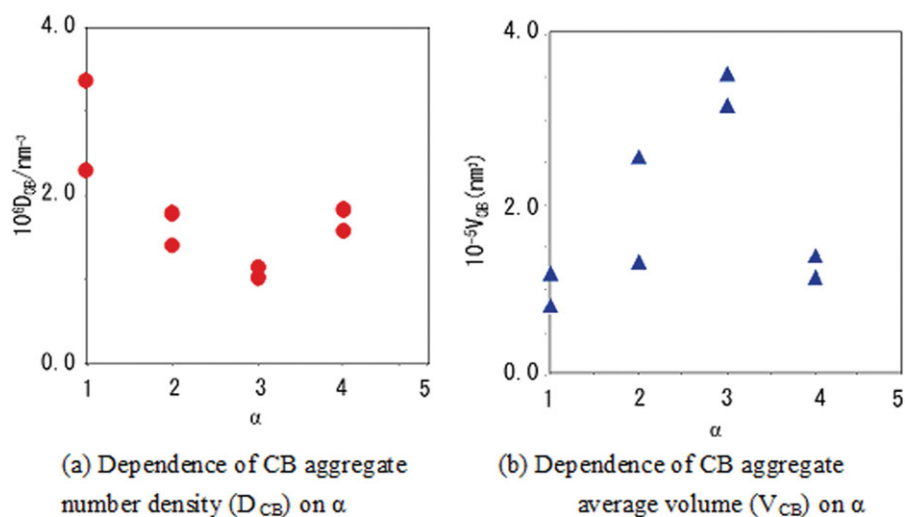


Figure 8. Dependence of  $D_{CB}$  and  $V_{CB}$  on  $\alpha$ . [Color figure can be viewed in the online issue, which is available at wileyonlinelibrary.com.]

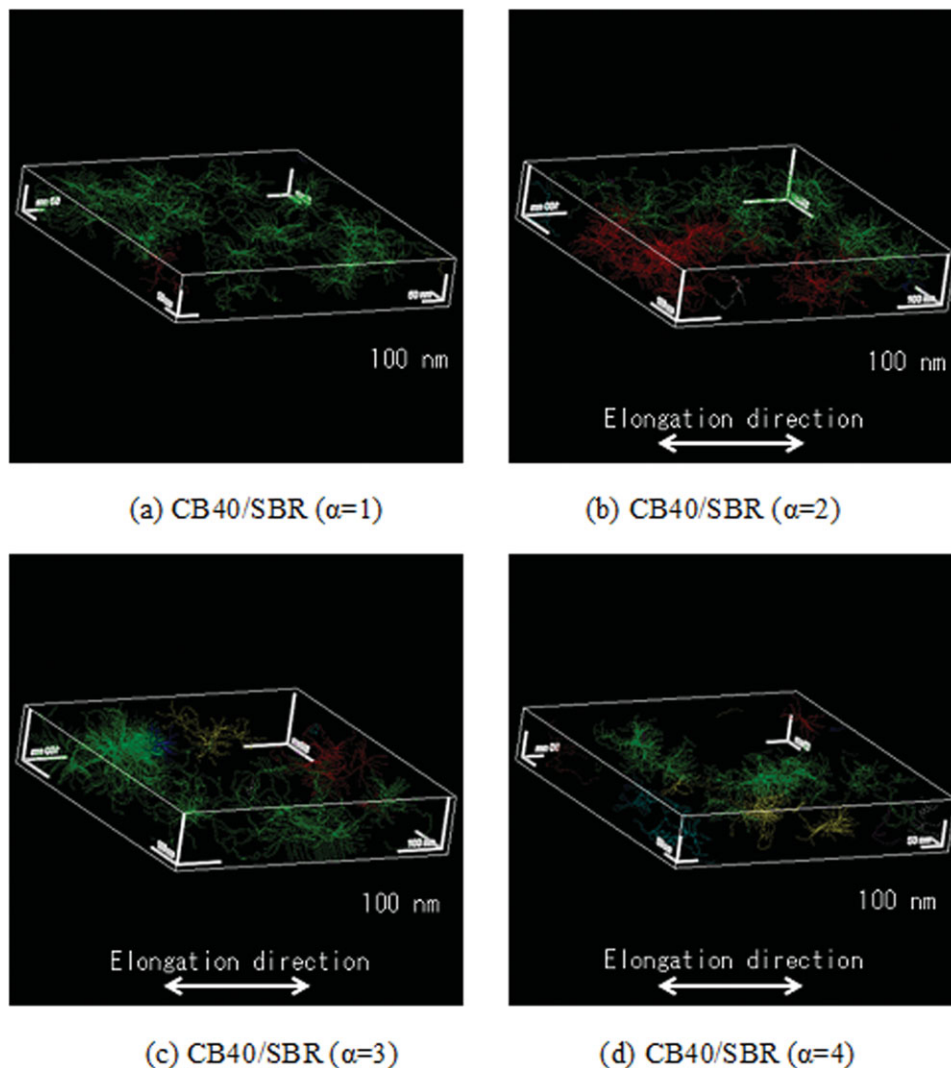
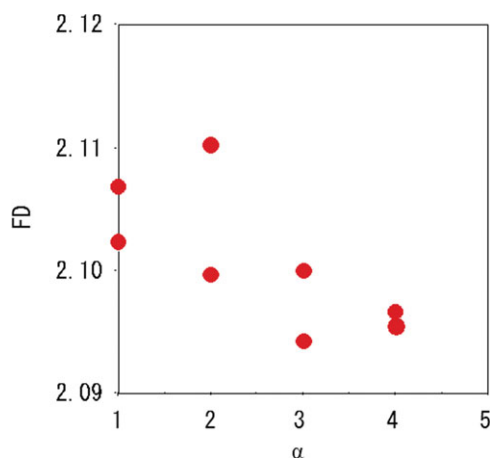


Figure 9.  $CB_{net}$  images of the CB-filled SBR samples cured in two steps. [Color figure can be viewed in the online issue, which is available at wileyonlinelibrary.com.]

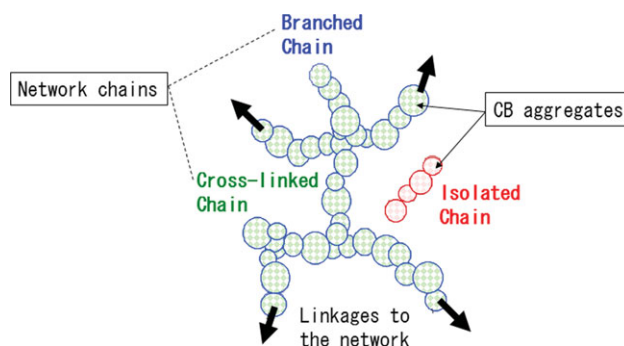


**Figure 10.** Relationship between the FD of  $CB_{net}$  and  $\alpha$ . [Color figure can be viewed in the online issue, which is available at [wileyonlinelibrary.com](http://wileyonlinelibrary.com).]

contrast, as the samples were increasingly elongated, the  $CB_{net}$  colors changed; this implied that the  $CB_{net}$  was broken by elongation. The CB40/SBR sample with  $\alpha = 4$  in Figure 9(d) in particular was broken up into small fragments.

In addition, the fractal dimension (FD) of the  $CB_{net}$  in Figure 9 was calculated by the box counting method.<sup>30–33</sup> FD of the  $CB_{net}$  is shown in Figure 10 as a function of  $\alpha$ . The results indicate that FD tended to decrease with increasing  $\alpha$ . This result suggests that the  $CB_{net}$  was flattened as a result of elongation.

The 3D network structure formed by the clustering of the  $CB_{ag}$ 's is schematically shown in Figure 11, together with the parameters of the network structures.<sup>7–12,14,24,26,27</sup> The circles in the figure represent the  $CB_{ag}$ 's. The thin arrows indicate that the CB chains composed of a few or several aggregates were linked to the surrounding network structures. The two thick arrows show



**Figure 11.**  $CB_{ag}$  network structure. [Color figure can be viewed in the online issue, which is available at [wileyonlinelibrary.com](http://wileyonlinelibrary.com).]

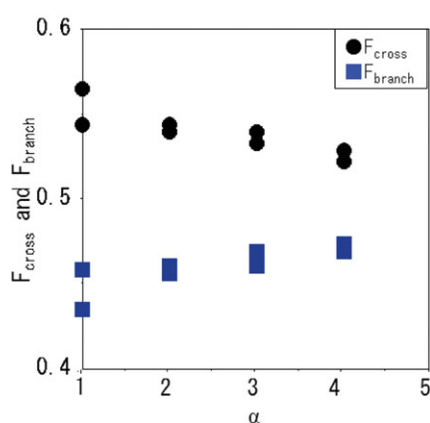
the crosslinking point ( $N_d$ ) and the branching point ( $T_m$ ) of the network, respectively. Presumably, this 3D network structure of the  $CB_{ag}$ 's was also closely related to various properties, in addition to the electrical characteristics. We noted that the branched chains and isolated chains of the  $CB_{ag}$ 's were observed in all of the samples that we examined. The  $CB_{net}$  parameters, that is, the fraction of crosslinked chains ( $F_{cross}$ ), fraction of branched chains ( $F_{branch}$ ), and fraction of isolated chains ( $F_{isolate}$ ), were defined by the following equations.<sup>7–14,23–27</sup>

$$F_{cross} = NN_d N_d / (NN_d N_d + NN_d T_m + NN_i) \quad (1)$$

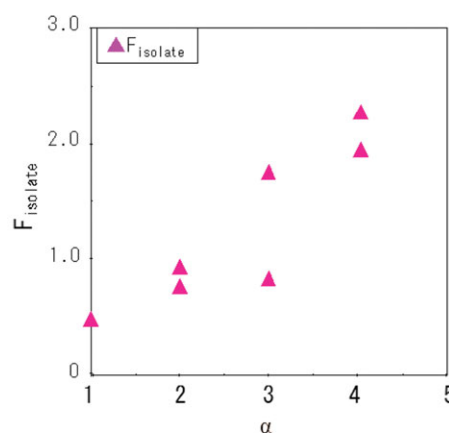
$$F_{branch} = NN_d T_m / (NN_d N_d + NN_d T_m + NN_i) \quad (2)$$

$$F_{isolate} = NN_i / (NN_d N_d + NN_d T_m + NN_i) \quad (3)$$

where  $NN_d N_d$  is the number of crosslinked chains,  $NN_d T_m$  is the number of branched chains,  $NN_i$  is the number of isolated chains, and  $NN_d N_d + NN_d T_m + NN_i$  is the total number of network chains. The three fractions shown in eqs. (1), (2), and (3) were the parameters used to characterize the  $CB_{net}$  structure.



(a) Dependence of fractions of cross-linked chain ( $F_{cross}$ ) and branched chain ( $F_{branch}$ ) on  $\alpha$



(b) Dependence of fraction of isolated chain ( $F_{isolate}$ ) on  $\alpha$

**Figure 12.** Dependence of the  $CB_{net}$  parameters on  $\alpha$ . [Color figure can be viewed in the online issue, which is available at [wileyonlinelibrary.com](http://wileyonlinelibrary.com).]



Figure 12 shows the dependence of  $F_{\text{cross}}$ ,  $F_{\text{branch}}$ , and  $F_{\text{isolate}}$  on  $\alpha$ . We observed that  $F_{\text{cross}}$  increased almost linearly and  $F_{\text{branch}}$  decreased almost linearly with increasing  $\alpha$ . These results suggest that the crosslinked chains of the  $\text{CB}_{\text{net}}$  were severed by elongation and the number of branched chains increased. Moreover, although  $F_{\text{isolate}}$  showed an overall tendency to increase with increasing  $\alpha$ , the increase was more pronounced in the region of  $3 < \alpha \leq 4$  than in the region of  $1 \leq \alpha < 3$ . These results imply that when elongation destroyed the  $\text{CB}_{\text{net}}$ , isolated chains were also generated in addition to branched chains and that the isolated chains were markedly generated in the region of  $\alpha < 3$ . In addition, the change in  $F_{\text{isolate}}$  around  $\alpha = 3$  corresponded closely to the aforementioned changes in  $\rho_v$  and  $\Delta E$  and to the changes in  $d_p$ ,  $d_g$ ,  $D_{\text{CB}}$ , and  $V_{\text{CB}}$  of the  $\text{CB}_{\text{ag}}$ 's.

## CONCLUSIONS

We observed that  $\rho_v$  of the CB40/SBR samples cured in two steps with  $\alpha$ s of 1–3, respectively, declined slightly, whereas  $\rho_v$  of the CB40/SBR sample with an  $\alpha$  of 4 increased markedly. These results imply that the electrical network of the  $\text{CB}_{\text{ag}}$ 's in the rubber was destroyed at  $\alpha = 4$ , that is, at an  $\alpha$  larger than 3.

On the other hand, the 3D TEM images of the CB40/SBR samples cured in two steps with  $\alpha$ s of 1–4, respectively, revealed that the gaps between the  $\text{CB}_{\text{ag}}$ 's tended to increase with increasing  $\alpha$ . The sample with an  $\alpha$  of 4 in particular showed that the  $\text{CB}_{\text{ag}}$ 's were broken apart. These results supported the pronounced increase in  $\rho_v$  for an  $\alpha$  of 4. Visualized images of the  $\text{CB}_{\text{net}}$  in the CB40/SBR samples cured in two steps with  $\alpha$ s of 1–4 showed that nearly all of the  $\text{CB}_{\text{ag}}$ 's were linked together at the closest  $d_p$  of approximately 3 nm in the unelongated state ( $\alpha = 1$ ). In contrast, in the elongated samples, we assumed that the  $\text{CB}_{\text{net}}$  was broken as a result of elongation. For the CB40/SBR sample with an  $\alpha$  of 4 in particular, we observed that the  $\text{CB}_{\text{net}}$  was broken up into small fragments. We found that the FD calculated with the box counting method tended to decrease with increasing  $\alpha$ . This result presumably indicated that the  $\text{CB}_{\text{net}}$  was flattened as a result of elongation. It was also found that  $F_{\text{cross}}$  of the  $\text{CB}_{\text{net}}$  increased nearly linearly with increasing  $\alpha$ , whereas  $F_{\text{branch}}$  decreased almost linearly. These results imply that the crosslinked chains of the  $\text{CB}_{\text{net}}$  were broken by elongation and that the number of branched chains increased. In contrast,  $F_{\text{isolate}}$  tended to increase overall with increasing  $\alpha$ ; the increase in  $F_{\text{isolate}}$  was more pronounced in the region of  $3 < \alpha \leq 4$  than in the region of  $1 \leq \alpha < 3$ . These results suggest that when the  $\text{CB}_{\text{net}}$  was destroyed by elongation, isolated chains were also generated in addition to the branched chains. The change seen in  $F_{\text{isolate}}$  around  $\alpha = 3$  corresponded closely to the aforementioned changes in  $\rho_v$  and  $\Delta E$  and also to the changes in  $d_p$ ,  $d_g$ , the coarsened  $\text{CB}_{\text{ag}}$ 's,  $D_{\text{CB}}$ , and  $V_{\text{CB}}$ .

The foregoing results imply that the  $\text{CB}_{\text{ag}}$ 's coarsened when the sample cross-sectional area at  $\alpha < 3$  decreased, and the destruction of the  $\text{CB}_{\text{net}}$  also proceeded gradually at the same time. In contrast, the coarsened  $\text{CB}_{\text{ag}}$ 's were finely divided at  $\alpha > 3$ , and the elongation presumably flattened and broke the

$\text{CB}_{\text{net}}$ . These results supported the marked decline observed in  $\rho_v$  at  $\alpha = 4$ .

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## REFERENCES

- Wei, L.; Tang, T.; Huang, B. *J. Polym. Sci. Part A: Polym. Chem.* **2004**, *42*, 941.
- Zhang, Q.; Archer, L. *Macromolecules* **2004**, *37*, 1928.
- Zhang, Q.; Archer, L. *Langmuir* **2002**, *18*, 10435.
- Steinstein, S. S.; Zhu, A. *Macromolecules* **2002**, *35*, 7262.
- Zhu, Z.; Thompson, T.; Wang, S. Q.; von Meerwall, E. D.; Halasa, A. *Macromolecules* **2005**, *38*, 8816.
- Ozsisik, R.; Zheng, J.; Dionne, P. J.; Picu, C. R.; von Meerwall, E. D. *J. Chem. Phys.* **2005**, *123*, 134901.
- Kohjiya, S.; Kato, A.; Shimanuki, J.; Hasegawa, T.; Ikeda, Y. *J. Mater. Sci.* **2005**, *40*, 2553.
- Kohjiya, S.; Kato, A.; Suda, T.; Shimanuki, J.; Ikeda, Y. *Polymer* **2006**, *47*, 3298.
- Kato, A.; Shimanuki, J.; Kohjiya, S.; Ikeda, Y. *Rubber Chem. Technol.* **2006**, *79*, 653.
- Ikeda, Y.; Kato, A.; Shimanuki, J.; Kohjiya, S.; Tosaka, M.; Poompradub, S.; Toki, S.; Hsiao, B. S. *Rubber Chem. Technol.* **2007**, *80*, 251.
- Kohjiya, S.; Ikeda, Y.; Kato, A. In *Current Topics in Elastomers Research*; Bhowmick, A. K., Ed.; CRC: Boca Raton, FL, **2008**; Chapter 19, p 543.
- Kohjiya, S.; Kato, A.; Ikeda, Y. *Prog. Polym. Sci.* **2008**, *33*, 979.
- Omnés, B.; Thuillier, S.; Pilvin, P.; Grohens, Y.; Guillet, S. *Compos. A* **2008**, *39*, 1141.
- Kato, A.; Suda, T.; Ikeda, Y.; Kohjiya, S. *J. Appl. Polym. Sci.* **2011**, *122*, 1300.
- Satoh, Y.; Fujii, S.; Kawahara, S.; Isono, Y.; Kagami, S. *e-J. Soft Mater.* **2007**, *3*, 29.
- Satoh, Y.; Suda, K.; Fujii, S.; Kawahara, S.; Isono, Y.; Kagami, S. *e-J. Soft Mater.* **2007**, *3*, 14.
- The Carbon Black Association, Japan. *Handbook of Carbon Black (in Japanese)*; The Carbon Black Association, Japan: Tokyo, **1995**; p 66.
- Nihon Gosei Gomu Co., Ltd. *JSR Handbook (in Japanese)*; JSR: Tokyo, **1985**; p 70.
- Kremer, J. R.; Mastrorarde, D. N.; McIntosh, J. R. *J. Struct. Biol.* **1996**, *116*, 71.
- Detlev, S.; Malte, W.; Hans-Christian, H. *The Visualization Handbook*; Ed. Hansen, C. D.; Johnson, C. R., Ed.; Elsevier: Amsterdam, New York and Rio de Janeiro, FL, **2005**, Chapter 38, p 749.
- Jinnai, K.; Nishi, T. *Microsc.* **2004**, *39*, 31 (in Japanese).
- Ikeda, Y.; Kato, A.; Shimanuki, J.; Kohjiya, S. *Macromol. Rapid Commun.* **2004**, *25*, 1186.
- Ikeda, Y. *Sen'I Gakkaishi* **2005**, *61*, 34.

24. Kato, A.; Ikeda, Y.; Kohjiya, S. *Nippon Gomu Kyokaishi* **2005**, *78*, 180.
25. Kohjiya, S.; Kato, A.; Shimanuki, J.; Hasegawa, T.; Ikeda, Y. *Polymer* **2005**, *46*, 4440.
26. Kohjiya, S.; Kato, A. *Kobunshi Ronbunshu* **2005**, *62*, 467.
27. Kato, A.; Kohjiya, S.; Ikeda, Y. *Kobunshi* **2006**, *55*, 616.
28. Kato, A.; Kohjiya, S.; Ikeda, Y. *Rubber Chem. Technol.* **2007**, *80*, 690.
29. Tsuji, M.; Fujita, M.; Kohjiya, S. *Nihon Reorogi Gakkaishi* **1997**, *25*, 193.
30. Hirata, M. *J. Appl. Polym. Sci.* **2000**, *78*, 1555.
31. Usui, M. H.; Ishizuki, M.; Shige, I.; Suzuki, H. *Korea–Aust. Rheol. J.* **2003**, *15*, 19.
32. Jäger, K.-M.; McQueen, D. H. *Polymer* **2001**, *42*, 9575.
33. Yuan, S.; Xu, H.; Gu, H. *J. Appl. Polym. Sci.* **2008**, *110*, 1955.